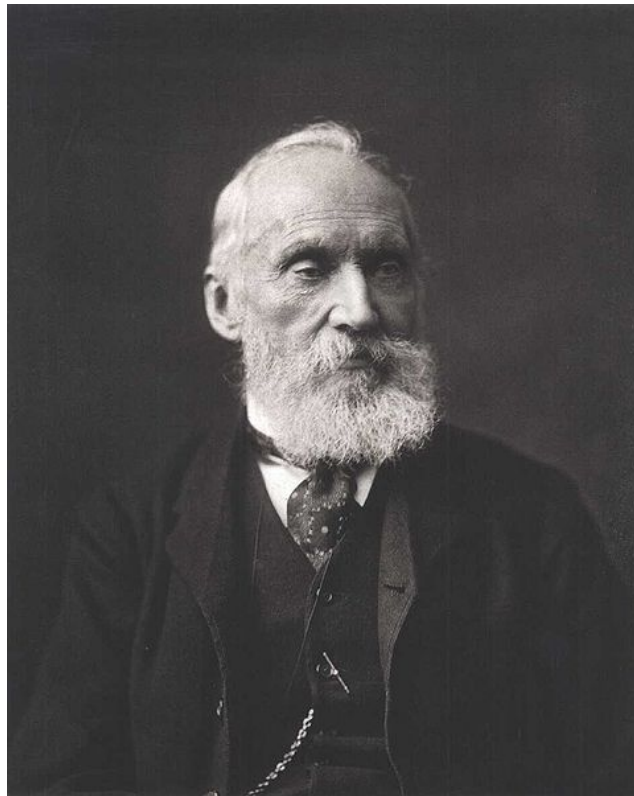


**GREEN'S THEOREM,
STOKES' THEOREM,
AND
GAUSS' THEOREM**



Recall Green's Theorem:

Theorem: Let C be a smooth, simple closed curve in the plane that is oriented counter-clockwise, and let R be the region bounded by C . If P and Q have continuous partial derivatives on an open region that contains R , then,

$$\int_C P dx + Q dy = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$$

If $\vec{F} = P\hat{i} + Q\hat{j}$ and $\vec{r}(t) = x(t)\hat{i} + y(t)\hat{j}$ is a smooth parametrization for C , then we can rewrite our equation as follows.

$$\begin{aligned} \text{Work} &= \int_C \vec{F} \cdot d\vec{r} = \\ &= \int_C P dx + Q dy = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA \end{aligned}$$

However, work is also a measure of circulation around a curve, and thus,

$$\begin{aligned}\text{Circulation} &= \int_C \vec{F} \cdot T \, ds = \int_C \vec{F} \cdot d\vec{r} \\ &= \int_C P \, dx + Q \, dy = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA \\ &= \iint_R (\text{curl } \vec{F}) \cdot \hat{k} \, dA = \iint_R (\nabla \times \vec{F}) \cdot \hat{k} \, dA\end{aligned}$$

This result is known as the 2-dimensional version of Stokes' Theorem.

$$\begin{aligned}\text{Circulation} &= \int_C \vec{F} \cdot T \, ds = \int_C \vec{F} \cdot d\vec{r} \\ &= \int_C P \, dx + Q \, dy = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA \\ &= \iint_R (\text{curl } \vec{F}) \cdot \hat{k} \, dA = \iint_R (\nabla \times \vec{F}) \cdot \hat{k} \, dA\end{aligned}$$

If we now go back to our parametrization for C ,

$\vec{r}(t) = x(t)\hat{i} + y(t)\hat{j}$ with $a \leq t \leq b$, then the unit

tangent is $T(t) = \frac{\vec{r}'(t)}{\|\vec{r}'(t)\|} = \frac{x'(t)}{\|\vec{r}'(t)\|}\hat{i} + \frac{y'(t)}{\|\vec{r}'(t)\|}\hat{j}$, and the

unit normal is $N(t) = \frac{y'(t)}{\|\vec{r}'(t)\|}\hat{i} - \frac{x'(t)}{\|\vec{r}'(t)\|}\hat{j}$.

Recall that the flux across the curve C produced by the force \vec{F} is $\int_C \vec{F} \cdot N ds$, and hence,

$$\begin{aligned}\text{Flux} &= \int_C \vec{F} \cdot N ds = \int_a^b (\vec{F} \cdot N) \frac{ds}{dt} dt \\ &= \int_a^b (P\hat{i} + Q\hat{j}) \cdot \left(\frac{y'(t)}{\|\vec{r}'(t)\|} \hat{i} - \frac{x'(t)}{\|\vec{r}'(t)\|} \hat{j} \right) \|\vec{r}'(t)\| dt \\ &= \int_a^b (P\hat{i} + Q\hat{j}) \cdot \left(\frac{dy}{dt} \hat{i} - \frac{dx}{dt} \hat{j} \right) dt = \int_a^b \left(P \frac{dy}{dt} - Q \frac{dx}{dt} \right) dt \\ &= \int_C P dy - Q dx = \int_C -Q dx + P dy = \iint_R \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} \right) dA \\ &= \iint_R \text{div } \vec{F} dA = \iint_R (\nabla \cdot \vec{F}) dA\end{aligned}$$

This result is known as the 2-dimension version of the Divergence Theorem or Gauss' Theorem.

$$\begin{aligned}\text{Flux} &= \int_C \vec{F} \cdot N \, ds = \int_a^b (\vec{F} \cdot N) \frac{ds}{dt} dt \\ &= \int_a^b (P\hat{i} + Q\hat{j}) \cdot \left(\frac{y'(t)}{\|\vec{r}'(t)\|} \hat{i} - \frac{x'(t)}{\|\vec{r}'(t)\|} \hat{j} \right) \|\vec{r}'(t)\| dt \\ &= \int_a^b (P\hat{i} + Q\hat{j}) \cdot \left(\frac{dy}{dt} \hat{i} - \frac{dx}{dt} \hat{j} \right) dt = \int_a^b \left(P \frac{dy}{dt} - Q \frac{dx}{dt} \right) dt \\ &= \int_C P dy - Q dx = \int_C -Q dx + P dy = \iint_R \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} \right) dA \\ &= \iint_R \text{div } \vec{F} \, dA = \iint_R (\nabla \cdot \vec{F}) \, dA\end{aligned}$$

To summarize, if $\vec{F} = P\hat{i} + Q\hat{j}$, C is a closed, counterclockwise oriented path parametrized by $\vec{r}(t) = x(t)\hat{i} + y(t)\hat{j}$, T is the unit tangent vector, and N is the unit normal vector, then:

GREEN'S THEOREM: $\text{Work} = \int_C \vec{F} \cdot d\vec{r} = \int_C P dx + Q dy = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$

STOKES' THEOREM: $\text{Circulation} = \int_C \vec{F} \cdot T ds = \int_C \vec{F} \cdot d\vec{r}$
 $= \int_C P dx + Q dy = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA = \iint_R (\text{curl } \vec{F}) \cdot \hat{k} dA = \iint_R (\nabla \times \vec{F}) \cdot \hat{k} dA$

GAUSS' THEOREM: $\text{Flux} = \int_C \vec{F} \cdot N ds = \int_C P dy - Q dx = \int_C -Q dx + P dy$
 $= \iint_R \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} \right) dA = \iint_R \text{div } \vec{F} dA = \iint_R (\nabla \cdot \vec{F}) dA$

In higher dimensions, Stokes' Theorem and Gauss' Theorem (the Divergence Theorem) look like this:

STOKES' THEOREM: Let S be an oriented piecewise-smooth surface that is bounded by a simple, closed, piecewise-smooth boundary curve C with positive orientation. Let \vec{F} be a vector field whose components have continuous partial derivatives on an open region in \mathbb{R}^3 that contains S . Then
$$\int_C \vec{F} \cdot d\vec{r} = \iint_S (\text{curl } F \cdot N) dS.$$

GAUSS' THEOREM: Let V be a solid region whose boundary surface S has positive (outward) orientation. Let \vec{F} be a vector field whose component functions have continuous partial derivatives on an open region that contains E . Then
$$\iint_S \vec{F} \cdot N dS = \iiint_V \text{div } \vec{F} dV$$

ENJOY!

